

PATENT ABSTRACTS OF JAPAN

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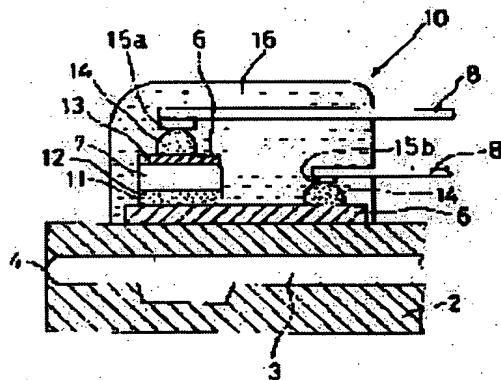
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(54) INK JET HEAD UNIT

(57)Abstract:

PURPOSE: To provide an ink jet head which has electrolytic corrosion resistance and being highly reliable through a long period of time and can be manufactured by a simple manufacturing method without requiring high cost.

CONSTITUTION: In an ink jet head which is manufactured by joining metal layers 6, electrically connected to a piezoelectric element 7, and wiring members 8 with a joining material 14 and is made up by molding with a sealing material 16 which covers the piezoelectric element 7 and the joining part, characteristic is constituted in such that when potential difference between the joining material 14 and the metal layers 6 is taken as ΔV (V) and water absorptivity of the sealing material 16 is taken as D (%), $\Delta V \times D \leq 1$.



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CLAIMS

[Claim(s)]

[Claim 1] An ink jet arm head characterized by being referred to as $\Delta V \times D \leq 1$ when a metal layer and a wiring member which are connected to a piezoelectric device and an electric target are joined by joint material, the potential difference of said joint material and metal layer is set to ΔV (V) in an ink jet arm head which carries out a mold and becomes so that said piezoelectric device and joint may be covered by closure member, and water absorption of said closure member is set to D (%).

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DETAILED DESCRIPTION

[Detailed Description of the Invention]

[0001]

[Industrial Application] This invention relates to the ink jet arm head used for the ink jet printer which prints by turning ink on record media, such as a form, and injecting it from a nozzle.

[0002]

[Description of the Prior Art] By making it come to arrange a piezoelectric device to the ink jet arm head formed in the shape of a nozzle in the point in the ink jet head unit, and energizing to a piezoelectric device based on predetermined printing timing, the ink jet arm head mentioned above is made to deform a piezoelectric device, decreases the cross section of the ink passage of an ink jet arm head, and prints by injecting the ink in an ink jet arm head from a nozzle, and making a form reaching the target.

[0003] Drawing 3 is the perspective diagram showing such a conventional ink jet arm head.

[0004] As shown in drawing 3, in the conventional ink jet arm head 1, two or more ink passage 3 and 3-- are formed in the interior of a substrate 2, the nozzle 4 which makes the side of the longitudinal direction in drawing of said substrate 2 breathe out ink is formed in one side of each of this ink passage 3, and the input 5 of ink is formed in another side. As shown in drawing 3, and on the whole surface of the outside of this substrate 2, i.e., the upper surface in drawing The metal layer 6 of the thin film applied as an electrode when the front face of a substrate 2 is lacking in conductivity is formed. To the pan of this metal layer 6 outside As it counters with said each ink passage 3, it is made to correspond to each ink passage 3, and the approximate circle board-like piezoelectric device 7 is joined by the jointing material which has conductivity so that the underside side may be connected electrically. The metal layer 6 formed in the base mentioned above also on the upper surface of this piezoelectric device 7 and the metal layer 6 of the same thin film are formed (not shown). The joint material in which the individual cable run section of the wiring members 8, such as a flexible print circuit (FPC), has conductivity through a conductor, For example, it fixes by the conductive paste which made solder, carbon, or a metallic material contain (not shown [both]), and one pole (usually anode plate) is constituted. Moreover, in the metal layer 6 on said substrate 2, the common cable run section of the wiring member 8 has fixed by said joint material (not shown) through the conductor as a pole (usually cathode) of another side. Thus, the wiring member 8 and the piezoelectric device 7 are electrically connected through the metal layer 6 and joint material of a thin film. And as shown in drawing 4, the mold of the joint of the metal layer 6 arranged on the whole surface of said substrate 2, each piezoelectric device 7, and the wiring member 8 is carried out by the closure member 9, and it is insulated to the exterior.

[0005] Moreover, the ink jet arm head it was made to make it contacted mechanically without making the wiring member 8 fix to these poles is also proposed.

[0006]

[Problem(s) to be Solved by the Invention] However, in the conventional ink jet arm head 1 mentioned above, as mentioned above, the metal layer 6 and the wiring member 8 of a thin film are joined through

joint material. And when the metal layer 6 and joint material of this thin film are the same material, it is very rare, and the case where the dissimilar material is used has the generality.

[0007] Therefore, between the metal layer 6 and joint material, the potential difference equivalent to the normal potential of this material will arise. And the moisture in atmospheric air adhered to the portion which this potential difference produced, electric corrosion occurred, and there was a trouble that the metal layer 6 of a thin film was destroyed by corrosion. Therefore, electric corrosion was made to prevent by using a corrosion-resisting material strong against corrosion for the metal layer 6, or devising the magnitude for a joint, and arrangement.

[0008] However, in the ink jet arm head 1 which performed such electric corrosion prevention, when a corrosion-resisting material was used, there was a trouble that the raw material itself will become expensive, and a manufacturing process became complicated and difficult. Furthermore, in order to have devised the magnitude for a joint, and arrangement, the critical point is arrived at by demand called high-performance-izing of today's ink jet arm head 1, and a miniaturization, and there was a trouble that it could not follow in footsteps of electric corrosion prevention.

[0009] Moreover, in the ink jet arm head it was made to make it contacted mechanically without making the wiring member 8 fix, although electric corrosion was not produced, since the contact force at the time of contact of the wiring member 8 affected ink discharge quantity, in the ink jet arm head of today's multi-nozzle format, there was a trouble that adjustment of the contact force mentioned above was difficult.

[0010] This invention is made in view of these points, and the trouble in the conventional thing mentioned above is conquered, and it continues at a long period of time, is reliable, without being an easy method and causing an economic burden, and aims at offering the ink jet arm head which can prevent electric corrosion easily.

[0011]

[Means for Solving the Problem] In order to attain the object mentioned above an ink jet arm head of this invention In an ink jet arm head which carries out a mold and becomes so that a metal layer and a wiring member which are connected to a piezoelectric device and an electric target may be joined by joint material and said piezoelectric device and joint may be covered by closure member When the potential difference of said joint material and metal layer is set to ΔV (V) and water absorption of said closure member is set to D (%), it is characterized by being referred to as $\Delta V \times D \leq 1$.

[0012]

[Function] When according to the ink jet arm head of this invention which consists of a configuration mentioned above the potential difference of joint material and a metal layer is set to ΔV (V) and water absorption of said closure member is set to D (%), by being referred to as $\Delta V \times D \leq 1$, adhesion of the moisture in the atmospheric air to the generating portion of the potential difference is intercepted by the closure member proper, and can prevent generating of electric corrosion certainly in a practical use region.

[0013]

[Example] Hereafter, drawing 1 explains the example of this invention.

[0014] Drawing 1 is drawing of longitudinal section of an important section showing one example of the ink jet arm head of this invention.

[0015] As shown in drawing 1, as for the ink jet arm head 10 of this example, the metal layer 6 of a thin film is formed in the front face of a substrate 2 by proper methods, such as vacuum evaporation and sputtering. As a raw material of this metal layer 6, the aluminum, nickel, chromium, etc. are suitable. And the piezoelectric device 7 is joined to the front face of this metal layer 6 with the substrate 2 and the opposed face 12 (drawing Nakashita side) which counters through the jointing material 11. and the conductor which the metal layer 6 of the same thin film as the front face of said substrate 2 is formed in the anti-opposed face 13 side which disagrees with the substrate 2 of a piezoelectric device 7, and was formed in this metal layer 6 through the joint material 14, such as conductive paste, at the end of the individual cable run section of the wiring members 8, such as a flexible print circuit (FPC), -- 15a is joined and the anode plate is constituted. As this joint material 14, since conductive pastes, such as

silver, nickel, and copper, are easy for workability, it is suitable.

[0016] Proper things, such as 2 liquid hybrid model of the epoxy system which has conductivity, are used for the jointing material 11 used for cementation to said metal layer 6 and piezoelectric device 7. In addition, this jointing material 11 is not especially limited to this example that what is necessary is just to have conductivity.

[0017] moreover, the conductor formed in the proper location of said metal layer 6 through the same joint material 14 as the above at the end of the common cable run section of the wiring member 8 -- 15b is joined and cathode is constituted.

[0018] Furthermore, the mold is carried out as each component part arranged on said metal layer 6 covers an outside by the closure member 16. What is necessary is just to choose from a well-known sealing material or adhesives suitably as this closure member 16, so that the conditions explained below may be suited.

[0019] That is, when the potential difference of said metal layer 6 and joint material 14 is set to ΔV (V) and water absorption of said closure member 16 is set to D (%), it is constituted so that it may be referred to as $\Delta V \times D \leq 1$.

[0020] In the ink jet arm head 10 which consists of a configuration mentioned above next, various kinds of potential difference was made to form combining the metal layer 6 and the joint material 14 with various raw materials, the mold was carried out by the various closure members 16, and the engine-performance experiment was conducted about the relation of the electric corrosion by the potential difference and water absorption. In this engine-performance experiment, the ink jet arm head 10 was held in the elevated-temperature thermostat of the temperature of 60 degrees C, and 95% of humidity, and the progress degree of electric corrosion was evaluated with time. Moreover, in consideration of the practical use range, when the ink jet arm head 10 was held for 90 days in the elevated-temperature thermostat of the temperature of 60 degrees C, and 95% of humidity, what does not have effect in a function was considered as acceptance.

[0021] Said engine-performance experimental result is shown in a table 1.

[0022]

表 1

○: 合格
×: 不合格

金属層 の素材	接合部材 の素材	接合部の 電位差 ΔV (V)	封止部材の 吸水率 D (%)	$\Delta V \times D$	接合部の電食の経時変化 (日)						
					30	60	90	120	150	180	210
Al	Ag	2.454	1.80	4.42	×						
			0.95	2.33	○	×					
			0.50	1.23	○	×	○	○	×		
			0.11	0.27	○	○	○	○	×		
	Ni	1.410	1.80	2.54	○	×					
			0.95	1.34	○	○	×	○	×		
			0.50	0.71	○	○	○	○	○	×	
			0.11	0.16	○	○	○	○	○	×	
	Cu	2.183	1.80	3.93	×						
			0.95	2.07	○	×					
			0.50	1.09	○	×	○	○	×		
			0.11	0.24	○	○	○	○	○		
	C	1.794	1.80	3.23	○	○	×				
			0.95	1.70	○	○	○	○	×		
			0.50	0.90	○	○	○	○	○	×	
			0.11	0.20	○	○	○	○	○	○	×
Ni	Ag	1.044	1.80	1.88	○	×					
			0.95	0.99	○	○	○	○	×		
			0.50	0.52	○	○	○	○	○	×	
			0.11	0.11	○	○	○	○	○	○	×
	Ni	0	1.80	0.00	○	○	○	○	○	○	○
			0.95	0.00	○	○	○	○	○	○	○
			0.50	0.00	○	○	○	○	○	○	○
			0.11	0.00	○	○	○	○	○	○	○
	Cu	0.733	1.80	1.32	○	○	×				
			0.95	0.70	○	○	○	○	○	○	○
			0.50	0.37	○	○	○	○	○	○	○
			0.11	0.08	○	○	○	○	○	○	○
	C	0.384	1.80	0.69	○	○	○	○	○	○	×
			0.95	0.36	○	○	○	○	○	○	○
			0.50	0.19	○	○	○	○	○	○	○
			0.11	0.04	○	○	○	○	○	○	○
Cr	Ag	1.536	1.80	2.76	○	×					
			0.95	1.46	○	×					
			0.50	0.77	○	○	○	×			
			0.11	0.17	○	○	○	○	○	×	
	Ni	0.492	1.80	0.89	○	○	○	○	○	×	
			0.95	0.47	○	○	○	○	○	○	○
			0.50	0.25	○	○	○	○	○	○	○
			0.11	0.05	○	○	○	○	○	○	○
Cr	Cu	1.265	1.80	2.28	○	×					
			0.95	1.20	○	○	○	×			
			0.50	0.63	○	○	○	○	○	○	×
			0.11	0.14	○	○	○	○	○	○	○
Cr	C	0.876	1.80	1.58	○	×					
			0.95	0.83	○	○	○	○	×		
			0.50	0.44	○	○	○	○	○	○	○
			0.11	0.10	○	○	○	○	○	○	○

What graph-ized a table 1 as relation of the electric corrosion by the potential difference and water absorption is shown in drawing 2.

[0023] It became clear that there was a clear principle in progress of the electric corrosion by the potential difference and water absorption by drawing 2 so that clearly. Namely, as mentioned above, when the potential difference of said metal layer 6 and joint material 14 is set to ΔV (V) and water absorption of said closure member 16 is set to D (%) The period which is not influenced [according /

the product of the potential difference and water absorption / to electric corrosion in ***** to zero] becomes long, and the effect by the electric corrosion to the ink jet arm head 10 can be easily removed certainly by constituting so that it may be referred to as $\Delta VxD \leq 1$.

[0024] Moreover, an economic burden can be reduced while being able to shorten the time amount which development of the ink jet arm head 10 takes, since it can follow in footsteps of various kinds of specifications accuracy and promptly by saying that conditional expression called $\Delta VxD \leq 1$ in the combination of said metal layer 6, joint material 14, and closure member 16 is changed.

[0025] In addition, this invention is not limited to said example and can be changed if needed.

[0026]

[Effect of the Invention] As explained above, when the potential difference of a metal layer and joint material is set to ΔV (V) for the combination of a metal layer, joint material, and a closure member and water absorption of a closure member is set to D (%), according to the ink jet arm head of this invention While the adverse effect to the ink jet arm head by electric corrosion is certainly [simplicity and] removable by constituting so that it may be set to $\Delta VxD \leq 1$, the extremely excellent effect that the flexibility of layout of an ink jet arm head can be raised is done so.

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DESCRIPTION OF DRAWINGS

[Brief Description of the Drawings]

[Drawing 1] Drawing of longitudinal section of an important section showing the ink jet arm head of this invention

[Drawing 2] Drawing showing the relation between the potential difference, water absorption, and electric corrosion

[Drawing 3] The perspective diagram of an important section showing the conventional ink jet arm head

[Drawing 4] The same drawing as drawing 3 which carried out the mold by the closure member

[Description of Notations]

2 Substrate

6 Metal Layer

7 Piezoelectric Device

8 Wiring Member

10 Ink Jet Arm Head

11 Jointing Material

14 Joint Material

16 Closure Member

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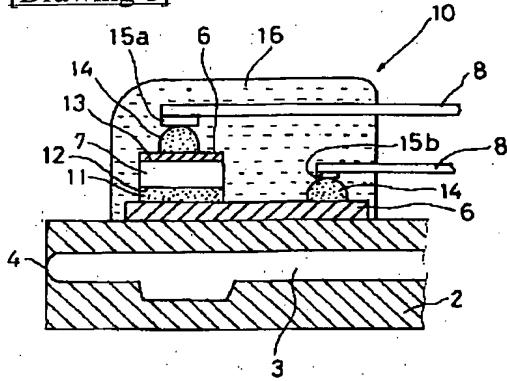
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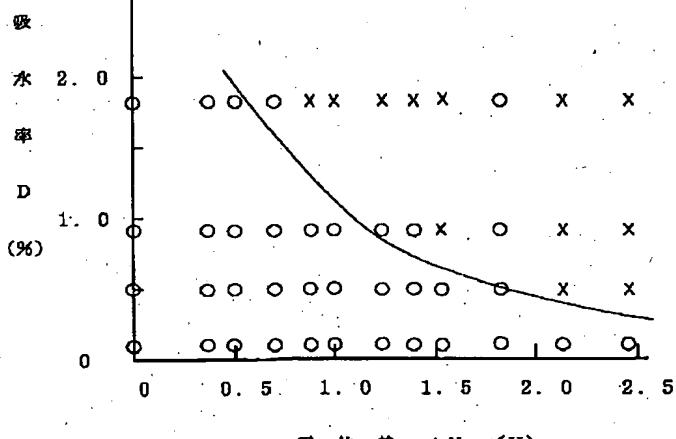
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DRAWINGS

[Drawing 1]

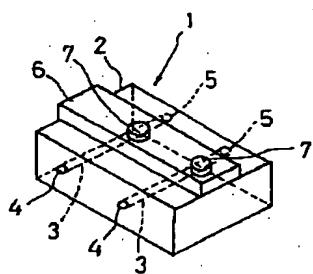


[Drawing 2]

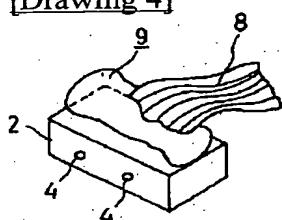


90日後の電食の評価結果 ○：合格 ×：不合格

[Drawing 3]



[Drawing 4]



[Translation done.]

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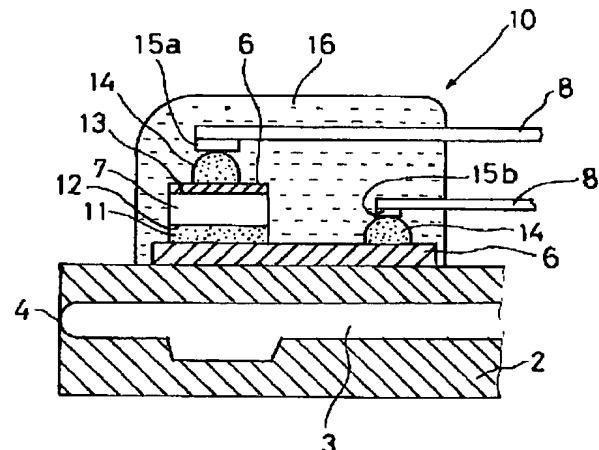
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(54)【発明の名称】 インクジェットヘッドユニット

(57)【要約】

【目的】 簡単な方法で、経済的負担を招くことなく、長期間に亘り信頼性が高く、容易に電食を防止できるインクジェットヘッドを提供する。

【構成】 圧電素子7と電気的に接続されている金属層6と配線部材8とを接合部材14により接合し、前記圧電素子7および接合部を封止部材16により覆うようにモールドしてなるインクジェットヘッドにおいて、前記接合部材14と金属層6との電位差を ΔV (V) とし、前記封止部材16の吸水率をD (%)としたときに、 $\Delta V \times D \leq 1$ としたことを特徴とする。



(3)

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$V \times D \leq 1$ としたことを特徴としている。

【0012】

【作用】前述した構成からなる本発明のインクジェットヘッドによれば、接合部材と金属層との電位差を ΔV (V) とし、前記封止部材の吸水率を D (%) としたときに、 $\Delta V \times D \leq 1$ とすることにより、電位差の発生部分への大気中の水分の付着が封止部材により適正に遮断され、電食の発生を実用域において確実に防止することができる。

【0013】

【実施例】以下、本発明の実施例を図1により説明する。

【0014】図1は、本発明のインクジェットヘッドの一実施例を示す要部の縦断面図である。

【0015】図1に示すように、本実施例のインクジェットヘッド10は、基板2の表面に蒸着およびスパッタリング等の適宜な方法により薄膜の金属層6が形成されている。この金属層6の素材としてはアルミニウム、ニッケル、クロム等が好適である。そして、この金属層6の表面には、圧電素子7が接着部材11を介して基板2と対向する対向面12(図中下面)をもって接合されている。そして、圧電素子7の基板2と相反する反対向面13側には、前記基板2の表面と同様の薄膜の金属層6が形成されており、この金属層6には導電ペースト等の接合部材14を介してフレキシブル・プリント・サーキット(FPC)等の配線部材8の個別電路部の一端に形成された導体15aが接合されて、陽極が構成されている。この接合部材14としては、銀、ニッケル、銅等の導電性ペーストが作業性が容易であるために好適である。

【0016】前記金属層6と圧電素子7との接合に用い

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る接着部材11には、導電性を有するエポキシ系の2液混合型等の適宜なものが用いられている。なお、この接着部材11は、導電性を有していればよく、特に、本実施例に限定されるものではない。

【0017】また、前記金属層6の適宜な位置には、前記と同一の接合部材14を介して配線部材8の共通電路部の一端に形成された導体15bが接合されて陰極が構成されている。

【0018】さらに、前記金属層6上に配置されたそれぞれの構成部品は封止部材16により外側を覆うようにしてモールドされている。この封止部材16としては、公知のシーリング材あるいは接着剤等から、つぎに説明する条件に適合するように適宜に選択すればよい。

【0019】すなわち、前記金属層6と接合部材14との電位差を ΔV (V) とし、前記封止部材16の吸水率を D (%) としたときに、 $\Delta V \times D \leq 1$ とさせるように構成されている。

【0020】つぎに、前述した構成からなるインクジェットヘッド10において、金属層6と接合部材14とを種々の素材により組み合わせて各種の電位差を形成させ、種々の封止部材16によりモールドして、電位差と吸水率とによる電食の関係について性能実験を行った。この性能実験においては、温度60℃、湿度95%の高温恒温槽内にインクジェットヘッド10を保持して、電食の進行程度を経時的に評価した。また、実用範囲を考慮して、温度60℃、湿度95%の高温恒温槽内にインクジェットヘッド10を90日間保持したときに機能に影響の無いものを合格とした。

【0021】表1に前記性能実験結果を示す。

【0022】

表 1

○: 合格
×: 不合格

金属層 の素材	接合部材 の素材	接合部の 電位差 ΔV (V)	封止部材の 吸水率 D (%)	$\Delta V \times D$	接合部の電食の経時変化 (日)						
					30	60	90	120	150	180	210
Al	Ag	2.454	1.80	4.42	×	×					
			0.95	2.33	○	×					
			0.50	1.23	○	×					
			0.11	0.27	○	○	○	×			
	Ni	1.410	1.80	2.54	○	×					
			0.95	1.34	○	○	×				
			0.50	0.71	○	○	○	×			
			0.11	0.16	○	○	○	○	×		
	Cu	2.183	1.80	3.93	×						
			0.95	2.07	○	×					
			0.50	1.09	○	×					
			0.11	0.24	○	○	○	×			
	C	1.794	1.80	3.23	○	○	×				
			0.95	1.70	○	○	○	×			
			0.50	0.90	○	○	○	○	×		
			0.11	0.20	○	○	○	○	○	○	×
Ni	Ag	1.044	1.80	1.88	○	×					
			0.95	0.99	○	○	○	×			
			0.50	0.52	○	○	○	○	×		
			0.11	0.11	○	○	○	○	○	○	×
	Ni	0	1.80	0.00	○	○	○	○	○	○	○
			0.95	0.00	○	○	○	○	○	○	○
			0.50	0.00	○	○	○	○	○	○	○
			0.11	0.00	○	○	○	○	○	○	○
	Cu	0.733	1.80	1.32	○	○	×				
			0.95	0.70	○	○	○	○	○	○	○
			0.50	0.37	○	○	○	○	○	○	○
			0.11	0.08	○	○	○	○	○	○	○
	C	0.384	1.80	0.69	○	○	○	○	○	○	○
			0.95	0.36	○	○	○	○	○	○	○
			0.50	0.19	○	○	○	○	○	○	○
			0.11	0.04	○	○	○	○	○	○	○
Cr	Ag	1.536	1.80	2.76	○	×					
			0.95	1.46	○	×					
			0.50	0.77	○	○	○	×	○	○	×
			0.11	0.17	○	○	○	○	○	○	○
	Ni	0.492	1.80	0.89	○	○	○	○	○	○	○
			0.95	0.47	○	○	○	○	○	○	○
			0.50	0.25	○	○	○	○	○	○	○
			0.11	0.05	○	○	○	○	○	○	○
	Cu	1.265	1.80	2.28	○	×					
			0.95	1.20	○	○	○	×	○	○	○
			0.50	0.69	○	○	○	○	○	○	○
			0.11	0.14	○	○	○	○	○	○	○
	C	0.876	1.80	1.58	○	×					
			0.95	0.83	○	○	○	×	○	○	○
			0.50	0.44	○	○	○	○	○	○	○
			0.11	0.10	○	○	○	○	○	○	○

表1を電位差と吸水率とによる電食の関係としてグラフ化したものを図2に示す。

【0023】図2により明白なように、電位差と吸水率とによる電食の進行には、明確な法則があることが判明した。すなわち、前述したように、前記金属層6と接合部材14との電位差を ΔV (V) とし、前記封止部材16の吸水率をD (%)としたときに、電位差と吸水率との積が零に近づくほど電食による影響を受けない期間が長くなり、 $\Delta V \times D \leq 1$ とさせるように構成することにより、容易にインクジェットヘッド10への電食による

影響を確実に除去することができる。

【0024】また、前記金属層6と接合部材14と封止部材16との組み合わせを $\Delta V \times D \leq 1$ という条件式を変更するということにより、各種の仕様に的確、かつ、迅速に追随できるので、インクジェットヘッド10の開発に要する時間を短縮させることができるとともに、経済的負担を低減させることができる。

【0025】なお、本発明は、前記実施例に限定されるものではなく、必要に応じて変更することができる。

【0026】

(5)

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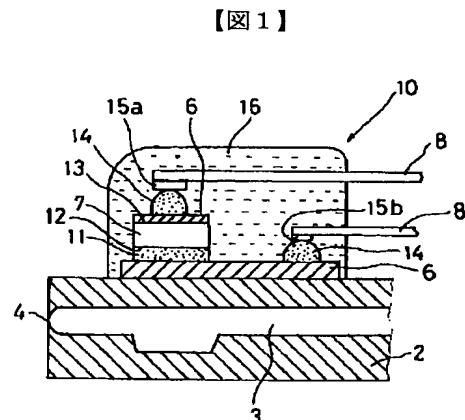
5

【発明の効果】以上説明したように本発明のインクジェットヘッドによれば、金属層と接合部材と封止部材との組み合わせを、金属層と接合部材との電位差を ΔV (V) とし、封止部材の吸水率をD (%)としたときに、 $\Delta V \times D \leq 1$ となるように構成することにより、電食によるインクジェットヘッドへの悪影響を、簡単、かつ、確実に除去することができるとともに、インクジェットヘッドの設計の自由度を向上させることができるという極めて優れた効果を奏する。

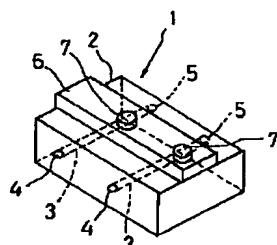
【図面の簡単な説明】

【図1】本発明のインクジェットヘッドを示す要部の縦断面図

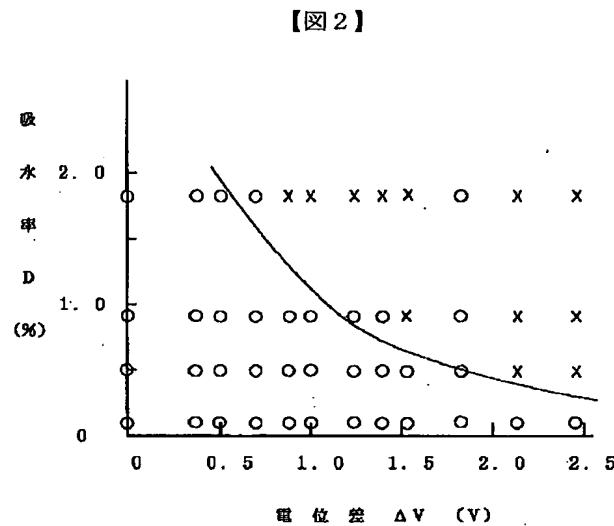
【図2】電位差と吸水率と電食との関係を示す図



【図3】



【図4】



90日後の電食の評価結果 ○：合格
×：不合格

